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London, EC4A 1PQ(GB)(54) **Thermoplastic resin-based molding composition.**

(57) A binary-blend molding resin composition based on a thermoplastic resin or polyolefin resin, e.g., polypropylene resin, which is capable of giving a molded article having improved mechanical properties, e.g., rigidity at an elevated temperature, and outer appearance as compared with conventional resin blends prepared by melt-blending comprises (A) a first thermoplastic resin, e.g., polypropylene, forming the matrix phase of the blend and (B) a second thermoplastic resin, e.g., polycarbonate resin, having a melting temperature higher than that of the component (A) or a thermosetting resin dispersed in the matrix of the component (A) retaining the particulate configuration of the unmolten resin powder having a specified average particle diameter and, preferably, a specified average aspect ratio, as prepared by the compounding work at a temperature at which the component (A) is melted but the component (B) is not melted. This composition is advantageous also when it is colored with a pigment because of the possibility of reducing the amount of the pigment to give a desired coloration to the shaped articles of the resin composition filled with a substantial amount of an inorganic filler having a masking power against the pigment.

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## THERMOPLASTIC RESIN-BASED MOLDING COMPOSITION

The present invention relates to a thermoplastic resin-based molding composition or, more particularly, to a polyolefin resin-based molding composition capable of giving molded articles having excellent appearance and various mechanical properties such as rigidity at high temperatures, dimensional accuracy of molding, resistance against whitening by scratches, yielding characteristics, and HDT (heat distortion temperature) so as to be useful as a molding material of various parts in automobiles, household electric appliances, information-processing equipment for office use and the like.

As is well known, polyolefin resins in general are widely employed as a molding material in the above mentioned application fields or as a material of films. One of the limiting factors against the application of polyolefin resins, however, is the relatively poor rigidity of the resin, in particular, at an elevated temperature.

Various attempts and proposals have been made hitherto in order to enhance the rigidity of a molded article of a polyolefin resin including a method of compounding the resin with a large amount of an inorganic filler such as calcium carbonate, talc, mica, asbestos, diatomaceous earth, glass fibers and the like; a method of blending the polyolefin resin with a polycarbonate resin, and so on.

The former method of compounding the resin with an inorganic filler is indeed effective in enhancing the rigidity of the shaped articles of the resin but several disadvantages are caused thereby such as an increase in the specific gravity of the shaped article, appearance of flow marks and silver streaks on the outer surface thereof and so on so that the method is not applicable when the shaped article should desirably have a low specific gravity or is desired to have attractive outer appearance.

In connection with the latter method of polymer blending with a polycarbonate resin, on the other hand, it is taught in Japanese Patent Kokai 59-223741 that a polypropylene resin is blended with a polycarbonate resin of the 4,4'-dihydroxy diphenyl alkane type in a molten state so that the polypropylene resin can be imparted with improved mechanical properties including rigidity at an elevated temperature. Although this method is indeed effective at least to some extent, several problems are unavoidable in the melt-blending of the resins due to the inherently poor compatibility of these two resins resulting in eventual delamination or separation into layers, in particular, in articles shaped by injection molding, so as to cause a degradation not only in the outer appearance but also in the mechanical properties of the shaped articles.

A remedial method for the above mentioned problem is proposed in Japanese Patent Kokai 59-223742 according to which the polypropylene resin per se to be melt-blended with a polycarbonate resin is a resin modified with an unsaturated carboxylic acid. This method, however, is not completely effective in improving the compatibility of the two different resins with the chemical interaction hardly taking place between the polycarbonate resin and the modified polypropylene resin leaving the above mentioned problem at least partly unsolved since the molecular chain terminals of a polycarbonate resin are usually blocked with a chain-end stopper or a molecular weight-controlling agent.

Further, attempts have been made in order to solve the above mentioned problems by compounding a thermoplastic resin with a powder of a different resin as a kind of filler. It is common, however, for the thus prepared resin composition to have rather poor yielding characteristics as compared with those of the base resin alone. This problem presents a great drawback against industrial development of organic-in-organic resinous composite materials.

The present invention provides, by solving the above mentioned problems in the prior art, a novel and improved thermoplastic resin-based molding composition or, in particular, a polyolefin resin-based binary molding composition comprising a polyolefin resin and a polycarbonate resin and capable of giving shaped articles having excellent outer appearance and mechanical properties without the risk of eventual occurrence of delamination or separation into layers.

The thermoplastic resin-based molding composition of the invention comprises, as a blend:

(A) from 50 to 99 parts by weight of a first thermoplastic resin; and

(B) from 50 to 1 part by weight of a second thermoplastic resin having a melting temperature higher than that of the first thermoplastic resin or a thermosetting resin, the first thermoplastic resin forming the matrix phase of the blend and the second thermoplastic resin or thermosetting resin forming a phase dispersed in the matrix of the first thermoplastic resin in the form of discrete particles having an average particle diameter in the range from 0.1 to 1000  $\mu\text{m}$ .

In particular, the component (A) is preferably a polyolefin resin or, more preferably, a polypropylene resin, and the component (B) is preferably a polycarbonate resin. Further, it is preferable that the particles of the component (B) have an average aspect ratio in the range from 1.0 to 10.0 or, more preferably, from 1.3 to 7.0.

As is described above, the resin composition of the present invention is characterized by the discrete dispersion of particles of the component (B) having a specified average particle diameter in the matrix of the component (A) in a specified weight proportion. By this means, the desired improvement in the properties of the resin composition can be well achieved disregarding the problem of compatibility between the components (A) and (B) compounded together.

Though not particularly limitative, the thermoplastic resin as the component (A) forming the matrix phase is preferably a polyolefin resin including homopolymers and copolymers of  $\alpha$ -olefins such as ethylene, propylene, butene-1, 3-methyl butene-1, 3-methyl pentene-1, 4-methyl pentene-1 and the like and copolymers of these olefins with other ethylenically unsaturated monomer or monomers copolymerizable therewith as well as blends of these polymers. Preferably, the component (A) is a polyethylene, a polypropylene or a combination thereof or, more preferably, a polypropylene in order to have the advantages of the invention exhibited most markedly.

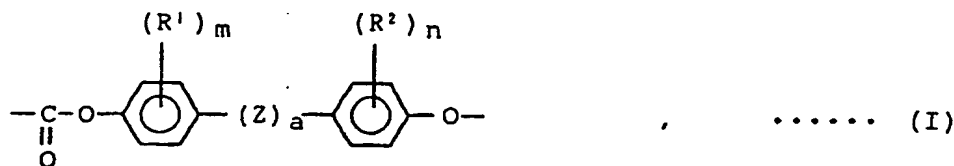
Various types of polyethylene resins can be used as the component (A) in the inventive resin composition including high-density, medium-density and low-density polyethylenes, linear low-density polyethylenes, ultra-high molecular-weight polyethylenes, copolymers of ethylene with another  $\alpha$ -olefin, copolymers of ethylene with vinyl acetate, copolymers of ethylene with an ester of acrylic acid and so on. Preferably, the polyethylene used as the component (A) is a high-density polyethylene having a melt index of 1 to 30 or a combination thereof with a minor amount of a polyethylene of other types.

Usable polypropylene resins as the component (A) include homopolymers of propylene, random and block copolymers of propylene with other  $\alpha$ -olefins copolymerizable with propylene and modified polypropylenes. Examples of preferable  $\alpha$ -olefins copolymerizable with propylene include those having 2 to 8 carbon atoms in a molecule such as ethylene, butene-1, pentene-1, hexene-1, heptene-1, octene-1 and the like, of which ethylene and butene-1 are more preferable. The copolymer of propylene should contain at least 60% by weight or, preferably, at least 70% by weight of the propylene moiety. Particularly preferable as the component (A) is a powdery block copolymer of propylene and ethylene of which the content of the ethylene moiety does not exceed 20% by weight. The polypropylene or propylene-based copolymer should preferably have a melt index of 0.05 to 4 g/10 minutes for a resin composition of the blow-molding grade and 3 to 60 g/10 minutes for a resin composition of the injection-molding grade though not particularly limited thereto.

It is optional that the component (A) in the inventive resin composition is a combination of a polypropylene and a polyethylene. The weight proportion of the polypropylene resin to the polyethylene resin should be in the range from 65:35 to 99:1 or, preferably, from 75:25 to 95:5.

Examples of thermoplastic resins other than the above mentioned polyolefin resins suitable as the component (A) include polyvinyl chloride-based resins, polyamide resins, e.g., 6-nylon, 6,6-nylon, 4,6-nylon, 6,10-nylon and 12-nylon, polyester resins, e.g., polyethylene terephthalate and polybutylene terephthalate, polycarbonate resins such as bisphenol A-based polycarbonate, aromatic polyethers and polythioethers, e.g., polyphenylene ethers, polyethylene ethers grafted with styrene, polyether ether ketones and polyphenylene sulfide, poly (aromatic ethers), e.g., polyoxybenzoyls and polyallylates, polysulfone resins, e.g., polyether sulfones and polyaryl sulfones, styrene-based resins, e.g., general-purpose polystyrenes, high-impact polystyrenes, polymers of  $\alpha$ -methyl styrene, copolymers of acrylonitrile, butadiene and styrene (ABS), copolymers of acrylonitrile and styrene (AS), copolymers of acrylonitrile, chlorinated polyethylene and styrene (ACS), copolymers of acrylonitrile, ethylene-propylene copolymeric rubber and styrene (AES) and copolymers of acrylic rubber, acrylonitrile and styrene (AAS), homopolymers and copolymers of (meth)acrylic acid esters, polyacetal resins, e.g., polyoxymethylene and formaldehyde-ethylene oxide copolymers obtained from trioxane and ethylene oxide, and the like.

The component (B) in the inventive resin composition can be a thermoplastic resin or a thermosetting resin. It is essential that, when the component (B) is a thermoplastic resin, the melting temperature of the component (B) is higher than that of the thermoplastic resin as the component (A) as in the combination of a polypropylene resin as the component (A) and a polycarbonate resin as the component (B) which is a preferable combination in the invention. Various types of polycarbonate resins can be used as the component (B) including aliphatic polycarbonate resins, aromatic polycarbonate resins and modified products thereof. Particular examples of the aromatic polycarbonate resin include those formed, at least partly, by the recurrence of the unit represented by the general formula



in which Z is a divalent atom or group selected from the class consisting of an oxygen atom, alkylene groups having 1 to 8 carbon atoms, alkylidene groups having 2 to 8 carbon atoms, cycloalkylene groups having 5 to 15 carbon atoms, cycloalkylidene groups having 5 to 15 carbon atoms, sulfonyl group, sulfoxide group, carbonyl group, sulfide group and a group expressed by the formula  $\text{-CMe}_2\text{-Pn-CMe}_2\text{-}$ , Me being a methyl group and Pn being a 1,4-phenylene group, the subscript a is zero or 1, R<sup>1</sup> and R<sup>2</sup> are each, independently from the others, a hydrogen atom, halogen atom or alkyl group having 1 to 8 carbon atoms and the subscripts m and n are each, independently from the other, a positive integer of 1 to 4.

These polycarbonate resins can be prepared in a well known procedure using methylene chloride and the like as the solvent by the reaction of a dihydric phenol and a carbonate precursor such as phosgen and the like in the presence of a known acid acceptor and a molecular-weight controlling agent or by the ester-exchange reaction between a dihydric phenol and a carbonate precursor such as diphenyl carbonate.

The above mentioned dihydric phenol is exemplified by 2,2-bis(4-hydroxyphenyl) propane or bisphenol A, 2,2-bis(3-methyl-4-hydroxyphenyl) propane, 2,2-bis(3,5-dimethyl-4-hydroxyphenyl) propane, 1,2-bis(4-hydroxyphenyl) ethane, 3,3-bis(4-hydroxyphenyl) pentane, 1,1-bis(4-hydroxyphenyl) cyclohexane, 4,4'-dihydroxy diphenyl, bis(4-hydroxyphenyl) sulfide, bis(4-hydroxyphenyl) sulfone, bis(4-hydroxyphenyl) sulfoxide, bis(4-hydroxyphenyl) ether, 4,4'-dihydroxy benzophenone and the like as well as halogenated bisphenol compounds such as 2,2-bis(3,5-dibromo-4-hydroxyphenyl) propane, 2,2-bis(3,5-dichloro-4-hydroxyphenyl) propane, 2,2-bis(3-chloro-4-hydroxyphenyl) propane, 2,2-bis(3-bromo-4-hydroxyphenyl) propane and the like, of which the first mentioned bisphenol A is particularly preferable. These dihydric phenol compounds can be used either singly or as a combination of two kinds or more according to need. Further, the polycarbonate resin as the component (B) can be a thermoplastic random-branched polycarbonate obtained by the combined use of a polyfunctional aromatic compound with the above mentioned dihydric phenol compound or can be a polymer blend of two kinds or more of polycarbonate resins of different types. The polycarbonate resin should preferably have a viscosity-average molecular weight in the range from 10,000 to 100,000 or, more preferably, from 20,000 to 100,000 in view of the effect of imparting a high mechanical strength to the shaped articles of the inventive resin composition.

It is further preferable to use a polycarbonate resin having crystallinity in view of the higher melting point of the resin than that of amorphous ones. Namely, the inventive resin composition comprising a crystalline polycarbonate resin can be shaped by molding without causing melting or deformation of the polycarbonate resin particles dispersed in the matrix at a relatively high molding temperature as compared with a molding composition compounded with particles of an amorphous polycarbonate resin of which the shaped articles may eventually be subject to a decrease in the HDT (heat-distortion temperature) or yield strength or occurrence of delamination.

Examples of other thermoplastic resins suitable as the component (B) include acrylate resins, polyallylate resins, polyethylene terephthalates, AS resins and the like.

Examples of thermosetting resins suitable as the component (B) include phenolic resins, urea resins, melamine resins, diallyl phthalate resins, unsaturated polyester resins, epoxy resins, polyimide resins, silicone resins and the like.

The inventive molding resin composition can be prepared by compounding, at a temperature such as not to cause melting of the component (B), the above described components (A) and (B) in such a proportion that the weight ratio of the component (A) to the component (B) is in the range of from 50:50 to 99:1 or, preferably, from 55:45 to 95:5 or, more preferably, from 65:35 to 90:10. When the weight proportion of the component (B) is too small, the desired effect of improving the rigidity of shaped articles at elevated temperatures cannot be fully exhibited as a matter of course. When the weight proportion of the component (B) is too large, on the other hand, the flowability of the resin composition may be impaired, together with a decrease in the impact strength of articles shaped from the resin composition. The compounding work of the components (A) and (B) is conducted, preferably, at a temperature at which the component (B) is not melted but the component (A) is in a molten state to facilitate uniform blending of the components.

The most characteristic feature of the inventive molding resin composition is that the component (B) forms a discretely dispersed phase in a particulate form in the matrix of the component (A) as a consequence of the compounding work being conducted at a temperature low enough not to cause melting

of the particles of the component (B). When the compounding work of the components is conducted at a temperature higher than the melting point of the component (B) or the resin composition is prepared by melt-blending of the components, the resin composition would give a shaped article which is eventually subject to the disadvantage of delamination, having poor outer appearance and poor mechanical properties.

5 The particles of the component (B) dispersed in the matrix of the inventive molding resin composition should have an average particle diameter in the range from 0.1 to 1000  $\mu\text{m}$  or, preferably, from 0.1 to 300  $\mu\text{m}$  or, more preferably, from 0.1 to 100  $\mu\text{m}$  in order that the desired effect by the compounding of the component (B) can be fully exhibited. It is further preferable that the particles of the component (B) dispersed in the matrix of the component (A) have a number-average aspect ratio in the range from 1.0 to  
10 10 or, more preferably, in the range from 1.3 to 7.

The molding resin composition of the present invention can optionally be compounded with various kinds of additives conventionally used in molding resin compositions according to need including, for example, inorganic fillers such as calcium carbonate, talc, mica, silica, asbestos and the like, fibrous reinforcing agents such as glass fibers, carbon fibers, metal whiskers and the like, antioxidants, ultraviolet  
15 absorbers, heat stabilizers, lubricants, flame retardants, antistatic agents and the like each in a limited amount.

The inventive molding resin composition can be prepared by uniformly blending the above described essential components (A) and (B) and the optional additives each in a specified proportion. The blending machine used in this compounding work is not particularly limitative, including Henschel mixers, single-screw or double-screw extruder machines, Banbury mixers and the like. The compounding work must be  
20 conducted at a controlled temperature sufficiently low not to cause melting of both of the components (A) and (B) or, preferably, at a temperature to cause melting of the component (A) but not to cause melting of the component (B) so that the particles of the component (B) in the matrix of the component (A) can retain their particle composition before compounding without being melted in the course of blending.

25 The inventive molding composition prepared in the above described manner can be molded by any conventional molding method including the extrusion molding method, injection molding method, blow molding method and the like without particular limitations. In any case, it is essential that the molding work is conducted at a temperature to cause melting of the component (A) but not to cause melting of the component (B) dispersed in a particulate form in the matrix of the component (A) so that the particles of the  
30 component (B) can retain the particle configuration before compounding with the component (A) even in the shaped articles of the resin composition.

Apart from the above described problems relative to the mechanical properties or, in particular, rigidity of the shaped articles of a thermoplastic resin-based molding composition at an elevated temperature, these thermoplastic resin-based molding compositions have another problem in respect of the colored appearance of shaped articles produced by compounding with a coloring pigment. Specifically, it is usual for a  
35 thermoplastic resin-based molding composition to be compounded with a substantial amount of an inorganic filler with an object to improve the mechanical properties, dimensional stability, heat resistance and the like of the shaped articles. When a shaped article of such a thermoplastic resin-based molding composition compounded with a substantial amount of an inorganic filler is desired to be colored by  
40 admixture of the molding composition with a pigment, sufficient coloration of the shaped article can be obtained only by greatly increasing the amount of the pigment due to the masking effect of the inorganic filler in reducing coloration by the pigment. In view of the increase in cost by increasing the amount of the relatively expensive pigment, it is highly desirable to develop a thermoplastic resin-based molding composition capable of giving a vividly colored shaped article having excellent dimensional stability and  
45 rigidity at an elevated temperature without compounding a large amount of an inorganic filler in which full coloration of the shaped article can be obtained with a relatively small amount of the compounded pigment.

In this regard, the present invention provides a solution for the above mentioned problem. When the thermoplastic resin-based molding composition composed of the above described components (A) and (B) according to the invention is compounded with a pigment with a view to coloration and the composition is  
50 molded into a shaped article, the thus obtained shaped article of the resin composition is imparted with full coloration even with a relatively small amount of pigment in addition to obtaining the great improvement in the mechanical properties in general as is described above.

The above mentioned improvement given by the present invention can be obtained with various kinds of organic and inorganic pigments without particular limitations. Examples of pigments usable in the  
55 invention include blue and green pigments such as phthalocyanine blue, phthalocyanine green, ultramarine, Prussian blue and the like, red and orange pigments such as quinacridone red, alizarin lake, thioindigo bordeaux, naphthol red, perylene red, polyazo red, dianthraquinonyl red, diketopyrrolopyrrole, perinone orange, red iron oxide and the like, yellow pigments such as isoindolinone yellow, quinophthalone yellow,

polyazo yellow, Hansa Yellow, Titan Yellow, lemon chrome, chrome yellow and the like, black pigments such as carbon black, anilin black, iron black and the like, white pigments such as titanium dioxide and the like, and so on. Two kinds or more of these pigments may be used in combination according to need. The amount of the pigment admixed in the inventive molding resin composition is in the range, usually, from 0.01 to 0.5% by weight or, preferably, from 0.05 to 0.3% by weight based on the total amount of the components (A) and (B) depending on the types of the pigments and the desired degree of coloration. It is sometimes advantageous that the pigment is compounded in the resin composition together with a metal soap or surface active agent as a dispersing agent.

When the resin composition comprising the components (A) and (B) is desired to be colored by the admixture of a pigment, it is important that the component (B) dispersed in the form of particles in the matrix of the component (A) has transparency as high as possible or, preferably, has a light transmission of at least 50% as determined according to the procedure specified in JIS K 1105 or a haze value not exceeding 20%.

In the following, the thermoplastic resin-based molding composition of the invention is described in more detail by way of examples, in which the term of "parts" always refers to "parts by weight". In the examples, evaluation of the resin compositions and the shaped articles molded therefrom was according to the following procedures and criteria.

(1) Melt index MI: according to the procedure specified in ASTM D-1238

(2) HDT: according to the procedure specified in ASTM D-648 under a load of 18.6 kg/cm<sup>2</sup>

(3) Density: according to the procedure specified in ASTM D-792

(4) Izod impact strength: according to the procedure specified in ASTM D-256

(5) Flexural yield strength: according to the procedure specified in ASTM D-790

(6) Molding shrinkage

A plate was prepared by injection molding of the resin composition using a one-end side-gate metal mold having dimensions of 420 mm (machine direction) × 100 mm × 2.5 mm and the machine-direction length  $L_{MD}$  in mm of the plate was measured. The molding shrinkage, %, was calculated from the following equation:

Molding shrinkage, % =  $(420 - L_{MD})/420 \times 100$ .

(7) Outer appearance

A plate sample of 420 mm × 100 mm × 2 mm dimensions prepared by injection molding of the resin composition was visually examined for the occurrence of flow marks and silver streaks and evaluated according to the following criteria.

A: absolutely no flow marks and silver streaks

B: few but not without flow marks and silver streaks

C: notable occurrence of flow marks and silver streaks

(8) Delamination

A pressure-sensitive cellophane-based adhesive tape was attached and bonded by pressing to the same injection-molded plate as prepared in (7) above at the portion around the gate and the tape was peeled off at a stretch to examine occurrence of delamination or separation into layers.

(9) Resistance against whitening by scratch

The surface of an injection-molded test piece of the composition having dimensions of 140 mm × 140 mm × 3 mm was scratched with the edge of a coin and the degree of whitening was visually evaluated in the following criteria.

A: absolutely no whitening

B: very little whitening

C: noticeable whitening

D: bad whitening

(10) Weld appearance

A test piece according to ASTM D-638 was prepared and conspicuousness of the center weld line was visually evaluated in the following criteria.

A: absolutely no weld line

B: very faint weld line

C: noticeable weld line

D: strong weld line

(11) Sink mark

A test piece having dimensions of  $\frac{1}{4}$  inch ×  $\frac{1}{2}$  inch × 5 inches according to the ASTM for the test of HDT was prepared by injection molding and visually inspected for the sink mark appearing on the  $\frac{1}{2}$  inch × 5 inches surface. The results were recorded according to the following criteria.

- A: absolutely no sink mark
- B: hardly noticeable sink mark
- C: noticeable sink mark
- D: very remarkable sink mark

5 (12) Surface condition

A test piece having dimensions of 420 mm X 100 mm 2 mm was prepared by injection molding and the surface was visually inspected for granular appearance due to the particles of the component (B), e.g., polycarbonate resin. The results were recorded according to the following criteria.

- A: absolutely no granular appearance
- 10 B: hardly noticeable granular appearance
- C: noticeable granular appearance
- D: very remarkable granular appearance

(13) Color development

15 The resin composition with admixture of 0.3% by weight of a brown pigment was kneaded and pelletized in an extruder machine and the pellets were injection-molded into a plate of which the degree of brown coloration was visually evaluated in three ratings of A for deep coloration, B for medium coloration and C for poor coloration.

(14) Color matching

20 The accuracy of color matching was given by the color difference  $\Delta E_{ab}^*$  determined according to the procedure specified in JIS K 7105 between a dark blue reference plate and the colored sample plate and given according to JIS Z 8730 (CIE-976). Practically, a value of  $\Delta E_{ab}^*$  smaller than 0.5 is required. The pigments used to exhibit dark blue color by blending included titanium dioxide, quinacridone magenta, phthalocyanine blue, carbon black and isoindolinone yellow and the pigments were used as a compound with 100 to 180% by weight of a metal soap.

25

Example 1.

30 Pellets of a resin composition were prepared, by blending at 200 °C in an extruder machine, 70 parts of a block-copolymeric polypropylene containing 6.5% by weight of ethylene moiety and having a melt index of 10 g/10 minutes (J-785H, a product by Idemitsu Petrochemical Co.) and 30 parts of a bisphenol A-type crystalline polycarbonate powder having a glass transition temperature of 154 °C and an average particle diameter of 500 μm. The temperature was sufficiently high to melt the block-copolymeric polypropylene but lower than the melting point of the polycarbonate resin. The pellets were injection-molded at 200 °C into a shaped body which was subjected to the various tests mentioned above to give the results shown in Table 1.

35

Example 2.

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The experimental procedure was exactly the same as in Example 1 above except that the polycarbonate particles had an average particle diameter of 200 μm. The results of the evaluation tests are shown in Table 1

45

Examples 3 to 6.

50 The experimental procedure in each of these examples was exactly the same as in Example 1 above except that the polycarbonate particles had an average particle diameter of 50 μm and the blending ratio of the polypropylene resin and the polycarbonate resin by weight was 70:30, 80:20, 92:8 and 60:40 in Examples 3, 4, 5 and 6, respectively. The results of the evaluation tests are shown in Table 1.

Comparative Example 1.

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The experimental procedure was exactly the same as in Example 1 above except that the polycarbonate powder was replaced with the same amount of pellets of the same polycarbonate resin. Each pellet had a cylindrical shape with a diameter of about 3 mm and a height of about 3 mm. The blend of the

polypropylene resin and the polycarbonate pellets could not be pelletized at 200 °C nor injection-molded.

#### Comparative Example 2.

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The experimental procedure was exactly the same as in Example 1 above except that the polycarbonate powder was replaced with the same amount of pellets of the same polycarbonate resin and the compounding work of the resin composition and injection molding of the composition were each conducted at 280 °C at which both of the polypropylene and polycarbonate resins were in a molten state. The results of the evaluation tests are shown in Table 1.

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#### Comparative Example 3.

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The same block-copolymeric polypropylene resin as used in Example 1 alone was injection-molded under the same molding conditions. The results of the evaluation tests are shown in Table 1.

#### Comparative Example 4.

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The experimental procedure was exactly the same as in Example 1 above except that the blending ratio of the polypropylene resin and the polycarbonate resin was 40:60 by weight. The results of the evaluation tests are shown in Table 1.

25

#### Comparative Example 5.

The experimental procedure was exactly the same as in Example 3 above except that the polycarbonate powder was replaced with the same amount of a calcium carbonate filler having an average particle diameter of about 3  $\mu\text{m}$ . The results of the evaluation tests are shown in Table 1.

30

Table 1

35			MI, g/10 minutes	HDT, °C	Delamination	Outer appearance	Density, g/cm <sup>3</sup>	Izod impact strength at 23 °C, kg·cm/cm
40	Example	1	8	75	No	B	0.97	4
		2	8	77	No	A	0.97	5
		3	8	80	No	A	0.97	6
		4	9	74	No	A	0.94	7
		5	10	66	No	A	0.92	8
		6	6	87	No	A	1.0	3
45	Comparative Example	2	8	76	Yes	C	0.97	2
		3	10	60	-	A	0.9	9
		4	3	96	No	B	1.06	2
		5	8	68	-	B	1.13	6
50								

55

#### Examples 7 to 11.

The experimental procedure in each of these examples was exactly the same as in Example 1 above



excepting the different temperature conditions in compounding and injection molding and different formulations relative to the average aspect ratio of the particles and amount of the polycarbonate powders each having an average particle diameter of 50  $\mu\text{m}$  including:

- 20 parts of crystalline resin particles having an average aspect ratio of 1.8 per 80 parts of the polypropylene in Example 7;
- 40 parts of crystalline resin particles having an average aspect ratio of 1.8 per 60 parts of the polypropylene in Example 8;
- 20 parts of crystalline resin particles having an average aspect ratio of 1.8 per 80 parts of the polypropylene in Example 9;
- 20 parts of crystalline resin particles having an average aspect ratio of 3.0 per 80 parts of the polypropylene in Example 10; and
- 20 parts of amorphous resin particles having an average aspect ratio of 1.8 per 80 parts of the polypropylene in Example 11.

The particle diameter mentioned above was determined and recorded as an average of the diameters along the major and minor axes of the particle.

The compounding work of the resin composition in each of these examples was conducted at 220 °C and the injection molding of the resin composition was conducted also at 220 °C in each of these examples excepting Example 9 in which the injection molding was conducted at 260 °C. The results of the evaluation tests are shown in Table 2.

#### Comparative Example 6.

The experimental procedure was exactly the same as in Example 1 except that the polypropylene resin alone was used without the polycarbonate resin and that the temperature in each of the compounding work and the injection molding of the resin composition was 220 °C instead of 200 °C. The results of the evaluation tests are shown in Table 2.

Table 2

		Flexural yield strength, kg/cm <sup>2</sup>	HDT, high °C	Molding shrinkage, t = 2.5 mm, %
Example	7	470	94	1.1
	8	510	105	0.7
	9	469	94	1.1
	10	490	97	1.0
	11	465	93	1.1
Comparative Example 6		430	67	1.7

#### Example 12.

Pellets of a resin composition were prepared, by blending at 220 °C in an extruder machine, 90 parts of the same block-copolymeric polypropylene as used in Example 1 and 10 parts of a bisphenol A-type crystalline polycarbonate powder having an average particle diameter of 30  $\mu\text{m}$  prepared by pulverization and particle size classification of a commercial product (FN-2200B, a product by Idemitsu Petrochemical Co.). The temperature was sufficiently high to melt the block-copolymeric polypropylene but lower than the melting point of the polycarbonate resin. The pellets were injection-molded at 220 °C into a shaped body which was subjected to the various tests mentioned above to give the results shown in Table 3.

Example 13.

The experimental procedure was exactly the same as in Example 12 except that 90 parts of the block-copolymeric polypropylene were replaced with a combination of 40 parts of the same block-copolymeric polypropylene, 40 parts of a homopolymeric polypropylene and 10 parts of a high-density polyethylene. The results of the evaluation tests are shown in Table 3.

Example 14.

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The experimental procedure was exactly the same as in Example 12 except that 90 parts of the block-copolymeric polypropylene were replaced with a combination of 80 parts of the same homopolymeric polypropylene and 10 parts of the same high-density polyethylene each as used in Example 13. The results of the evaluation tests are shown in Table 3.

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Example 15.

The experimental procedure was exactly the same as in Example 12 except that the weight ratio of the block-copolymeric polypropylene and the polycarbonate powder was 80:20 instead of 90:10. The results of the evaluation tests are shown in Table 3.

Example 16.

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The experimental procedure was exactly the same as in Example 15 except that 80 parts of the block-copolymeric polypropylene were replaced with a combination of 70 parts of the same block-copolymeric polypropylene and 10 parts of the same high-density polyethylene as used in Example 13. The results of the evaluation tests are shown in Table 3.

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Comparative Example 7.

The experimental procedure was exactly the same as in Example 16 excepting replacement of the polycarbonate powder with the same amount of the same polycarbonate pellets as used in Comparative Example 1. The results of the evaluation tests are shown in Table 3.

Comparative Example 8.

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The experimental procedure was exactly the same as in Example 15 except that 80 parts of the block-copolymeric polypropylene resin were replaced with a combination of 40 parts of the same block-copolymeric polypropylene and 40 parts of the same high-density polyethylene as used in Example 13. The results of the evaluation tests are shown in Table 3.

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Comparative Example 9.

The experimental procedure was exactly the same as in Example 16 except that the polycarbonate powder was replaced with the same amount of talc having an average particle diameter of about 2  $\mu\text{m}$ . The results of the evaluation tests are shown in Table 3.

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Table 3

		Density g/cm <sup>3</sup>	MI, g/10 minutes	Izod impact strength, kg*cm/cm	HDT, low, °C	Molding shrinkage, t = 2.5 mm, %	Resistance against whitening by scratch	Surface condition	Weld appearance	Sink mark	Flow mark	Color development
Example	12	0.92	20	5	122	1.3	A	B	A	B	A	A
	13	0.92	18	6	122	1.3	A	B	A	B	A	A
	14	0.92	22	4	128	1.3	A	B	A	B	A	A
	15	0.95	17	4	130	1.1	B	B	A	A	A	A
	16	0.95	15	6	126	1.1	A	B	A	A	A	A
	7	0.95	17	6	126	1.1	C	C	B	A	B	B
Comparative Example	8	0.95	12	10	101	1.2	A	B	B	A	C	A
	9	1.04	16	10	124	1.1	D	B	C	C	D	C

Example 17.

5       The experimental procedure was exactly the same as in Example 4 except that the resin composition was further admixed with 0.11 part of a pigment blend composed of 7.5% by weight of quinacridone magenta, 74.1% by weight of phthalocyanine blue and 18.4% by weight of carbon black and the compounding work and injection molding were conducted each at 220 °C. The pigments were introduced  
10      in the form of a blend with 100-180% by weight of a metal soap as a dispersing agent prepared beforehand. The results of the evaluation tests are shown in Table 4.

Example 18.

15       The experimental procedure was exactly the same as in Example 17 except that the polycarbonate powder had an average particle diameter of 100 µm instead of 50 µm and the amount of the pigment blend was increased to 0.14 part. The results of the evaluation tests are shown in Table 4.

20      Example 19.

      The experimental procedure was exactly the same as in Example 17 except that the weight proportion of the polypropylene to the polycarbonate powder was 90:10 instead of 80:20 and the amount of the  
25      pigment blend was increased to 0.13 part. The results of the evaluation tests are shown in Table 4.

Comparative Example 10.

30       The formulation of the resin composition was the same as in Example 18 except that the amount of the pigment blend, which was composed of 1.8% by weight of titanium dioxide, 4.7% by weight of quinacridone magenta, 71.9% by weight of phthalocyanine blue and 21.6% by weight of carbon black, was increased to 0.64 part but the compounding work was conducted at 300 °C so that the polycarbonate particles could no longer retain the particulate configuration in the composition. The results of the evaluation tests are shown  
35      in Table 4.

Comparative Example 11.

40       The experimental procedure was exactly the same as in Comparative Example 10 except that the polycarbonate powder was replaced with the same amount of polycarbonate pellets. The results of the evaluation tests are shown in Table 4.

45      Comparative Example 12.

      The experimental procedure was exactly the same as in Example 17 except that the polycarbonate powder was replaced with the same amount of talc and a pigment blend, which was composed of 17.0% by weight of titanium dioxide, 4.8% by weight of quinacridone magenta, 63.9% by weight of phthalocyanine  
50      blue and 14.3% by weight of carbon black, was used in an amount of 0.65 part. The results of the evaluation tests are shown in Table 4.

Comparative Example 13.

55       A colored resin composition was prepared by compounding 100 parts of the same polypropylene resin as used in Example 17 and 0.19 part of a pigment blend, which was composed of 42.8% by weight of titanium dioxide, 0.3% by weight of quinacridone magenta, 41.7% by weight of phthalocyanine blue and

15.2% by weight of carbon black, at 220 °C and injection-molding the composition also at 220 °C. The results of the evaluation tests are shown in Table 4.

Table 4

		Color matching, $\Delta$ $E_{ab}^*$	Density g/cm <sup>3</sup>	MI, g/10 minutes	Molding shrinkage, t = 2.5 mm, %	HDT, high, °C
Example	17	0.15	0.94	10	1.0	76
	18	0.20	0.94	10	1.1	75
	19	0.14	0.92	11	1.3	72
Comparative Example ple	10	0.20	0.94	6	1.1	75
	11	0.21	0.94	6	1.1	74
	12	0.17	1.04	9	1.1	75
	13	0.18	0.90	10	1.6	68

## Claims

1. A thermoplastic resin-based molding composition which comprises, as a blend:
  - (A) from 50 to 99 parts by weight of a first thermoplastic resin; and
  - (B) from 50 to 1 part by weight of a second thermoplastic resin having a melting temperature higher than that of the first thermoplastic resin or a thermosetting resin, the first thermoplastic resin forming the matrix phase of the blend and the second thermoplastic resin or thermosetting resin forming a phase dispersed in the matrix of the first thermoplastic resin in the form of discrete particles having an average particle diameter in the range from 0.1 to 1000  $\mu$ m.
2. A thermoplastic resin-based molding composition as claimed in claim 1 wherein the component (A) is a polyolefin resin and the component (B) is a polycarbonate resin.
3. A thermoplastic resin-based molding composition as claimed in claim 2 wherein the component (A) is a polypropylene resin.
4. A thermoplastic resin-based molding composition as claimed in any preceding claim wherein the particles of the component (B) dispersed in the matrix phase of the component (A) have an average particle diameter in the range from 0.1 to 300  $\mu$ m.
5. A thermoplastic resin-based molding composition as claimed in any preceding claim wherein the particles of the component (B) dispersed in the matrix phase of the component (A) have an average aspect ratio in the range from 1.0 to 10.
6. A thermoplastic resin-based molding composition as claimed in claim 5 wherein the particles of the component (B) dispersed in the matrix phase of the component (A) have an average aspect ratio in the range from 1.3 to 7.
7. A method for the preparation of a thermoplastic resin-based molding composition which comprises the step of uniformly blending
  - (A) from 50 to 99 parts by weight of a first thermoplastic resin; and
  - (B) from 50 to 1 part by weight of a second thermoplastic resin having a melting temperature higher than that of the first thermoplastic resin or a thermosetting resin in the form of a powder having an average particle diameter in the range from 0.1 to 1000  $\mu$ m,
 at a temperature at which the component (A) is melted but the component (B) is not melted so that the component (A) forms the matrix phase of the blend and the component (B) forms a phase dispersed in the matrix of the first thermoplastic resin in the form of discrete particles having an average particle diameter in the range from 0.1 to 1000  $\mu$ m.
8. A method for the preparation of a thermoplastic resin-based molding composition as claimed in claim 7 wherein the component (A) is a polyolefin resin and the component (B) is a polycarbonate resin.
9. A method for the preparation of a thermoplastic resin-based molding composition as claimed in claim 8

wherein the component (A) is a polypropylene resin.

10. A colored thermoplastic resin-based molding composition which comprises, as a blend:

(A) from 50 to 99 parts by weight of a first thermoplastic resin;

5 (B) from 50 to 1 part by weight of a second thermoplastic resin having a melting temperature higher than that of the first thermoplastic resin or a thermosetting resin having transparency, and

(C) a colored pigment in an amount sufficient for coloration of the blend,

the first thermoplastic resin forming the matrix phase of the blend and the second thermoplastic resin or thermosetting resin forming a phase dispersed in the matrix of the first thermoplastic resin in the form of discrete particles having an average particle diameter in the range from 0.1 to 1000  $\mu\text{m}$ .

10 11. A colored thermoplastic resin-based molding composition as claimed in claim 10 wherein the component (B) has a light transmission of at least 50% according to JIS K 1105.

12. Use of a thermoplastic resin-based molding composition as claimed in any one of claims 1 to 6 or 10 or 11, or when made by a method as claimed in any one of claims 7 to 9, in the manufacture of molded articles of manufacture.

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